



IT'S A TRAP!

**MICHIGAN CONCRETE
CANOE TEAM**

DESIGN REPORT 2011



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EXECUTIVE SUMMARY

A long time ago, in a galaxy far, far away, a great voice spoke, leaving the world trembling in their seats. Darth Vader’s eponymous voice reverberates in the minds of tens, if not hundreds, of millions people. From “I am your father” to “escape is not his plan,” we at the University of Michigan know all too well the true strength behind these words.

At the University of Michigan, we take great pride in our history, in the people who came before us and established the precedence for excellence and determination. The University established its College of Engineering in 1854, offering courses in civil engineering. Since its founding, the College has pioneered new technologies, theories, and groundbreaking research. The Michigan Concrete Canoe Team (MCCT) has had a presence within the Civil Engineering Department since 1992, just four years after the founding of the ASCE National Concrete Canoe Competition, and has been an active participant ever since. The team was revived by a group of dedicated civil engineering students, who had heard about the University of Michigan’s participation in several regional competitions in the 1970’s. During its years of competition, MCCT has

consistently placed fourth or fifth overall at regional competition.

This year, MCCT strove to incorporate more sustainable building practices during the fabrication of the canoe to reduce our impact on the environment. The team made use of a male mold for construction, which allowed for a reduction in foam sheets and thus waste. Haydite and Bionic Bubbles were selected as sustainable materials, as Haydite is expanded shale, and Bionic Bubbles are a by-product of coal-combustion. Through the use of more recycled materials, sustainable construction techniques and minimization of waste, MCCT hopes to be a strong contender at this year’s competition.

<i>It's a Trap!</i>	
Weight	258.3 lbs
Length	20 ft
Width	2 ft 7.2 in
Depth	1 ft 4 in
Hull Thickness	3/4 in
Concrete Colors	Grey / White
Concrete Unit Weight	55.51 lb/ft ³ / 64.22 lb/ft ³
Compressive Strength	1461 psi / 1546 psi
Reinforcement	Fiber Glass Mesh

Table 1: Canoe Specifications

As hosts of this year’s North Central Regional Conference, we will not let up against the competition. The Alliance feared the power and cunning of the Dark Side, leading Admiral Ackbar to famously announce, “*It's a Trap!*” It is after this statement that MCCT has named their 2011 canoe, whose specifications are listed in **Table 1**. This year, we will not sit idly by as other teams come into our house. Through exercise regimens and canoe training, we hope to present a real challenge to our opponents; may the force be with them.



ANALYSIS

MCCT analyzed the primary bending stresses on *It's A Trap!* using several different programs. The canoe was modeled by extrapolating from the provided lines drawing using Rhinoceros 4.0. The curves were imported from AutoCAD to create a hull surface. The hull was given an interior thickness of 3/4 inch, a 3/4 inch internal gunwale support, and a 3/4 inch centerline rib, which extends along the innermost 8 feet of the canoe, a cross section of which is shown in Figure 1. The gunwale supports

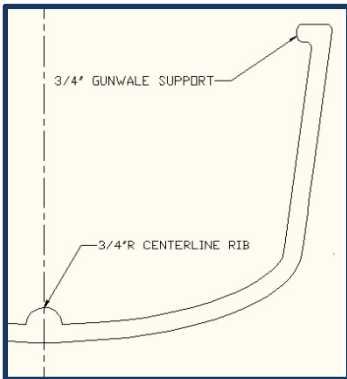


Figure 1: Hull Diagram and centerline rib increase the moment of inertia of the canoe, thereby decreasing the stress on the points furthest from the neutral axis. Sectional areas and mass properties of the canoe were determined at 20 points along the length of the canoe. Using curves of best fit to interpolate values between the points, we calculated the section modulus and stresses on the gunwales and keel of the canoe. Mathematical models based on the curves of best fit approximated the mass distribution, neutral axis and moments of inertia. These models were also used to find the distance from the neutral axis to the gunwales and keel, and the section modulus as a function of position.

The canoe hull was imported from Rhinoceros into Formation Design Systems' Maxsurf Pro Suite, which generated a hydrostatic model of the hull. In Hydromax Ultimate, part of the Maxsurf Suite, five individual load cases were defined, one for each of the race configurations. Male paddlers were conservatively approximated to weigh 180 pounds, and female paddlers approximated at 140 pounds. The canoe weight was calculated to be 258.3 pounds using the mass distribution obtained in Rhinoceros, with a longitudinal centroid of 10 feet

2.26 inches from the bow. Paddlers were spaced such that the canoe would trim by the stern to ensure that the centroid of the underwater profile would be aft of the center of gravity, and thus the canoe would be dynamically stable and naturally tend to travel on a straight course. Hydromax then determined equilibrium draft and trim for each load case and generated net force, shear force and moment curves for the canoe under each load case, as shown in Figure 2. The bending moments for each of the five load cases were converted to stress on the gunwales and keel and the maximum stresses on each were compared.

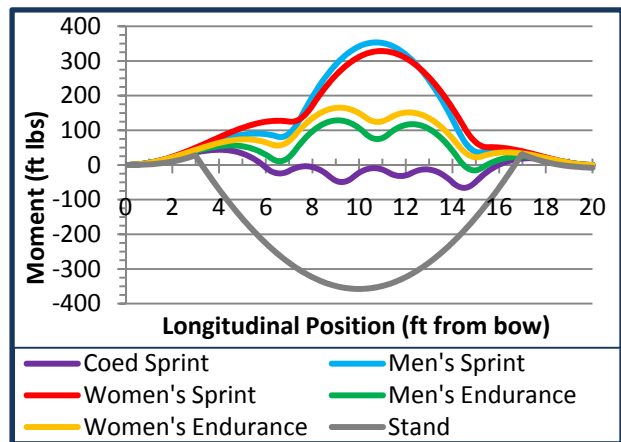


Figure 2: Loading Case Bending Moments

It was determined that the keel undergoes a maximum tensile stress of 26.41 psi and a maximum compressive stress of 25.16 psi (simply supported and men's sprints configurations, respectively). Likewise, the gunwales undergo a maximum tensile stress of 51.87 psi and a maximum compressive stress of 54.17 psi (men's sprints and simply supported configurations, respectively). Therefore, MCCT designed the mixes for *It's A Trap!* to attain a target composite tensile yield strength of 104 psi with mesh, and a compressive yield strength of 108 psi, allowing a safety factor of 2. MCCT is confident that the canoe will not suffer from local failures, based on both the thickness of the canoe and previous years' calculations.



DEVELOPMENT AND TESTING

MCCT's primary goal this year was to design a lightweight concrete that was both workable and sustainable by intelligently replacing previous materials with more sustainable and innovative materials. The mix design for *Wolverine* was used as a baseline because of its successful performance in the construction of last year's canoe. MCCT also sought to build upon the successful research and testing techniques developed while designing the mix for last year's canoe, *Wolverine*.

The 14-day compressive strength of the baseline mix was approximately 600 psi. The baseline cementitious materials in *Wolverine*'s mix design included Type 1 white Portland cement, Ground Granulated Blast Furnace Slag (GGBFS), and Silica Fume. This year, Silica Fume was replaced with rice husk ash (RHA) for several reasons. First, as a by-product of the rice-milling industry, RHA is an inexpensive and locally available recycled material. RHA also results in black colored concrete, which lends itself well to this year's Star Wars theme. As a locally available by-product of steel production, GGBFS was once again used as a recycled cementitious material.

More significant changes took place this year in selecting aggregates, which MCCT did by conducting research, perusing past winning reports and consulting with material companies, graduate students and professors. The primary goal of this research was to find an alternative for the crushed concrete used in the previous year's mix. The baseline aggregates for last year's mix included recycled crushed concrete, three sizes of Poraver, and K-15 glass microspheres. The crushed concrete was the densest of the three and had the largest particle size. To remedy this, MCCT replaced crushed concrete with finely graded Haydite – a sustainable material, and a better fit within the mix. This decision, coupled with that to use Bionic Bubbles and only two sizes of Poraver (0.25-0.5mm, and 0.5-1mm), improved the workability of this year's concrete. This also ensured better bonding between concrete layers, as the aggregate

particles could better fill the openings in the mesh reinforcement.

Five separate test batches of concrete were mixed, with varying proportions of RHA, Bionic Bubbles, PVA fibers and water. The RHA was varied to determine how its proportioning affected the overall concrete strength and wetness (as RHA requires more water than other cementitious materials to hydrate). MCCT was able to increase the water content of the concrete to meet the requirements of RHA due to the elimination of the previous rule limiting water content. After testing, MCCT found the optimum amount of RHA to be 15% by weight of the cementitious materials. The fiber content was varied and the subsequent workability of the concrete evaluated, the goal being to decrease the amount of fibers, improving workability while maintaining the concrete's tensile strength. The optimum amount of fiber was found to be approximately half of that used in last year's mix.



Figure 3: Two Test Batches. Because all five concrete batches proved to be equally workable and had approximately equivalent densities, strength was the deciding factor for the final mix design.

MCCT chose to use the same fiberglass mesh reinforcement as had been used for *Wolverine* for several reasons. First, the mesh had a very high strength to weight ratio and had been successful in preventing significant cracking in *Wolverine*. Second, the mesh had an open area of 50%, allowing for adequate bonding between layers of concrete. Finally, the team was able to use the excess mesh from the construction of

Wolverine, cutting cost and reducing construction waste by utilizing already available materials.

The final admixture selection changed very little from the baseline mix. Neither the MSDS nor the latex product information sheet provided a recommended dosage. Super-plasticizer was used according to the manufacturer recommended dosage range of 195-390mL/100kg of cement, while the air entraining agent used the dosage recommended.

PROJECT MANAGEMENT

This year, MCCT had a budget of \$4000 for the total cost of the project; \$700 was set aside for any unforeseen and emergency expenses. The rest of budget was allocated towards concrete materials, construction materials, reinforcement materials, recruiting, transportation, competition registration and miscellaneous expenses. The current projected cost for the materials is approximately \$3400, so the team is well within the budget. This however is not the final figure, since some of the potential costs have not yet been incurred.

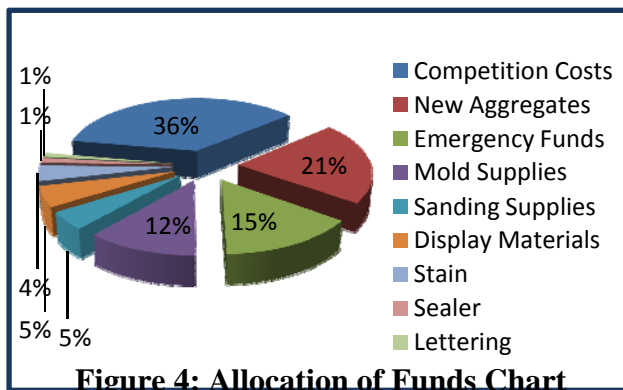


Figure 4: Allocation of Funds Chart

The project officially started on September 7, 2010 with a team leadership meeting, returning member meeting, and the official start of recruitment. However, team leaders had also kept in contact throughout the summer, discussing ways to improve the team organization. The team was able to begin researching aggregates and developing a mold as soon as the NCCC rules were released.

The team adopted a more rigorous schedule, one which would have resulted in a pour day in early December. However, due to setbacks in mold fabrication, pour day was moved to the first weekend in January, 29 days ahead of the previous year and 37 days ahead of the year before that. The project is currently scheduled to be completed on March 21, 2011, after which the team will practice in the completed canoe. At the end of the year MCCT plans to hold one final meeting in order to assess the team's ability to meet its goals and the areas upon which need to be improved.

In the overall organization for the project, the work was divided into two separate divisions: Research and Development, and Construction. Senior team members were elected to lead each division and oversee the newer members. Each division leader divided the work as he or she saw fit, delegating tasks to the newer members while explaining the methods and techniques the team has used in the past. The overall team focus shifted as workload changed, with most team members working primarily on Research and Development in the fall, and then shifting to Construction in winter and early spring. The team leadership believes that experience within multiple aspects of the project will lead to a better understanding of the problems at hand, a greater understanding of engineering as a whole, and more capable team leaders in the future.

Learning from previous years' struggles, team leadership identified potential issues within the project, including concrete placement, sample testing, and paddling techniques. The team conducted a practice placement session to allow new members to become familiar with the techniques used in construction. The team continued to test sample batches of concrete which systematically varied individual components to determine optimum proportions. Mixes were designed based on a database of previous aggregates and mix designs. The entire team was encouraged to attend mixing and testing sessions to allow for an increased understanding of the mix



design process. Additionally, all team members were safety trained and familiarized with ASTM standard testing procedures. Canoe paddling practices and weekly workout sessions were held throughout the year, and will culminate in several paddling practices using *It's a Trap!*

Major activities during the project could be classified into two groups: Milestone activities and Critical Path events. Milestone activities are considered to be those that, once initiated, mark the beginning of the change from one phase of the project to the next. The following Milestone activities were identified:

- Recruit New Members
- Research Aggregate Materials
- Mix & Test Sample Batches
- Cut & Assemble Mold
- Place Canoe
- Demold & Sand Canoe
- Stain & Seal Canoe
- Create Display & Stand
- Competition

Critical Path activities were those constrained by the availability of certain facilities or the completion of a prior stage of construction. The critical path activities are as follows:

- Mass Meeting
- Cut Foam Mold
- Place Canoe
- Demold Canoe
- Submit Technical Paper
- Paddling Practice

Cutting the foam mold, one of the most important critical path activities was heavily constrained by the availability of the CNC router used to cut the foam and the ensuing critical path activity “Place Canoe.” The activity “Place Canoe” was also considered critical and considered to have zero total float, since any delay would leave insufficient time for finishing work on the canoe.

The total number of man-hours is split into three major divisions and is summed up to the total man-hours spent by the team on the project:

- Research and Development (includes aggregate, mesh, pigments and plasticizer research, testing, preparing test cylinders, and documenting research findings): 75 man hours
- Construction (includes creating 3-D model of canoe, preparing cut-paths, scheduling foam cutting router, cutting foam sheets, assembling and finishing the mold, pouring the canoe, and finishing-testing): 540 man hours
- Recruitment (includes work done during summer and prior to school re-opening, creating team website, scheduling MCCT’s presence in college events, editing sending out sponsorship letters, and arranging team-bonding events): 50 man hours

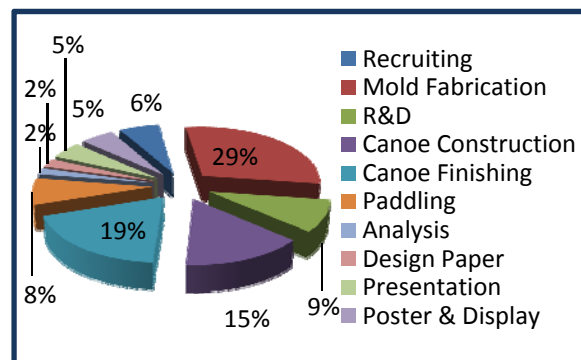


Figure 5: Man Hours Break Down

CONSTRUCTION

This year’s construction method differed from the previous two years in that the team chose to use a male mold. The male mold made the concrete easier to place, mitigating the effects of slump on canoe thickness while forcing the team to take special care in maintaining concrete thickness and exterior surface quality. A 3-D model of the canoe mold was created using Rhinoceros 4.0 and then



sliced into 120 two inch thick sections along its length. The resulting sections of 3D surface were then organized to fit on 4' by 8' foam sheets and cut using a CNC router. Key holes were cut into each section such that 2x4's could be used for alignment during mold assembly, along with 1/2



Figure 6: CNC Cutting Mold

sections were cut three-dimensionally to within 1/32 of an inch using a spherically tipped drill bit.

Once cut, the mold was aligned on several tables which had been lined up end to end and leveled to prevent any twisting of the mold. The mold sections themselves were aligned using both 2x4's and a laser sight and glued together with guerrilla glue. The mold was lightly sanded and drywall compound was used to fill in any gaps between sections. The entire exterior of the mold was covered with duct tape to allow for easier demolding and a smoother interior finish.

On pour day, approximately 14 ten-liter batches of concrete were mixed and progressively placed on the mold in two 3/8 inch layers. Once a sufficient length of the first layer of concrete was placed, a section of mesh was placed on top and the second layer of concrete was placed on top of the mesh. To ensure the thickness of each layer remained constant, several team members were given the task of quality control. Numerous pins with markings at 3/8 and 3/4 inch were used to verify canoe thickness throughout. The concrete was placed on the mold by hand with the first layer receiving little compaction to ensure sufficient concrete bonding through the mesh. Between the two layers of concrete, 2 foot long sections of fiberglass mesh were placed with six inches of

inch diameter sight holes as a means of checking alignment with a laser sight. To ensure the absolute accuracy of the mold, all

overlap. Six inches of overlap was determined in previous years to be sufficient to prevent weak spots in the tensile strength of the canoe. The mesh was placed in 2 foot sections for easier handling, and to avoid cold joints between layers. The second layer of concrete was compacted and smoothed with trowels.



Figure 7: Concrete Placement

After placing, the canoe was wet-cured in a heated environment for fourteen days. Once cured, the exterior was thoroughly sanded and then the canoe was carefully demolded. The interior was sanded and the canoe was stained and sealed in accordance with the Star Wars theme. The canoe was swamp tested to determine whether or not additional floatation was necessary.

MCCT considered safety to be of utmost importance in the construction and finishing



Figure 8: Sanding with Respirators

members were required to attend safety training classes prior to working in laboratory facilities, and were required to use personal protective equipment, including safety glasses, respirators and gloves during mixing, placing and sanding. OSHA was contacted prior to sanding to ensure the safest working conditions.

This year MCCT strove to create a high quality product through improvements to previous years' techniques, while creating an environment in which



newer members could learn from more experienced ones. This resulted in a more unified team, which worked together to solve problems better than any before.

INNOVATIONS AND SUSTAINABILITY

MCCT had specific goals for innovation this year. These goals included: developing a construction method that ensured the proper and accurate assembly of the canoe mold, centralizing the team's construction and finishing activities, and increasing the amount of sustainable materials used in the concrete mix design.

MCCT made many strides this year in improving construction techniques, particularly to the process of mold assembly. In



Figure 9: Mold on Levelled Tables

past years, MCCT

had erroneously assumed that the mold was being constructed on a level surface, aligned along a straight section of 2x4's. This year, MCCT made



Figure 10: Sight Holes

no such assumptions. Several tables were arranged end to end and levelled to create a flat, raised surface upon which to align the mold and construct the canoe. The individual mold sections were aligned using 1/2

inch diameter sight holes that ran the length of the mold, in conjunction with a laser sight. Having the canoe at waist level also increased productivity and quality control while placing concrete.

This year, instead of placing the canoe in the University of Michigan Civil Engineering structures lab, then transporting it to a separate location for finishing, MCCT utilized the University of Michigan's Walter E. Wilson Student Team Project Center as the location for all canoe construction and finishing. This allowed the team to mix, place, sand, stain, and seal all in one location, cutting down on time spent transporting the canoe between buildings.

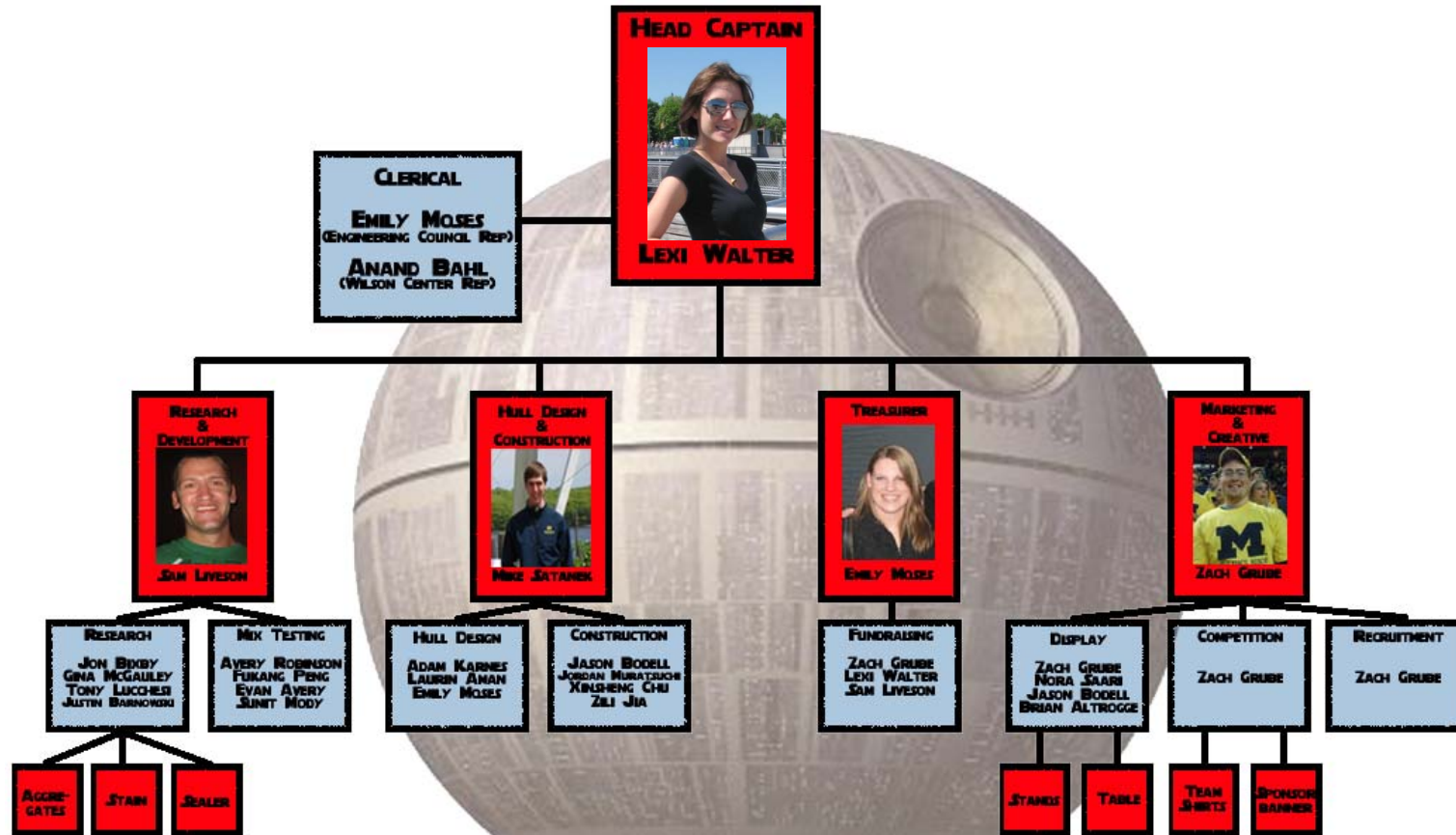
MCCT spent a great deal of time researching and testing materials for use in this year's concrete mix; these efforts led to the incorporation of Bionic Bubbles, rice husk ash (RHA), and Haydite. Bionic

Figure 11: MCCT Working in the Wilson Center

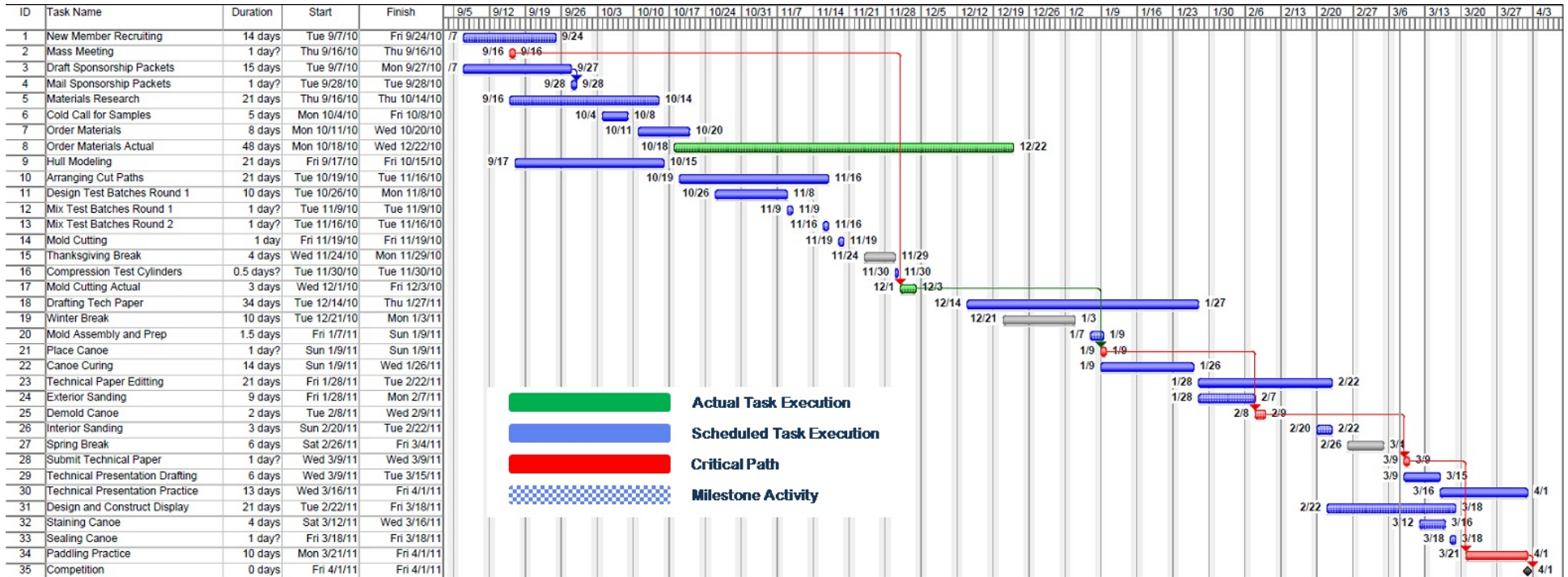
Bubbles are fine ceramic spheres made from a byproduct from coal combustion. RHA is the ash created from burning rice husk as a fuel for the processing of paddy. The ash is usually dumped in the surrounding environment, but can be used in concrete as a pozzolan – thereby reducing waste and harm to the environment. Haydite is expanded shale and is considered sustainable as it reduces the volume of material needed to be mined, and the amount of energy used in transportation. These aggregates, in conjunction with the use of Poraver (a recycled glass microsphere), Ground Granulated Blast Furnace Slag (a locally available byproduct of steel production), allowed MCCT to create a mix with 92% sustainable aggregate and 50% sustainable cementitious materials.



Organizational Chart

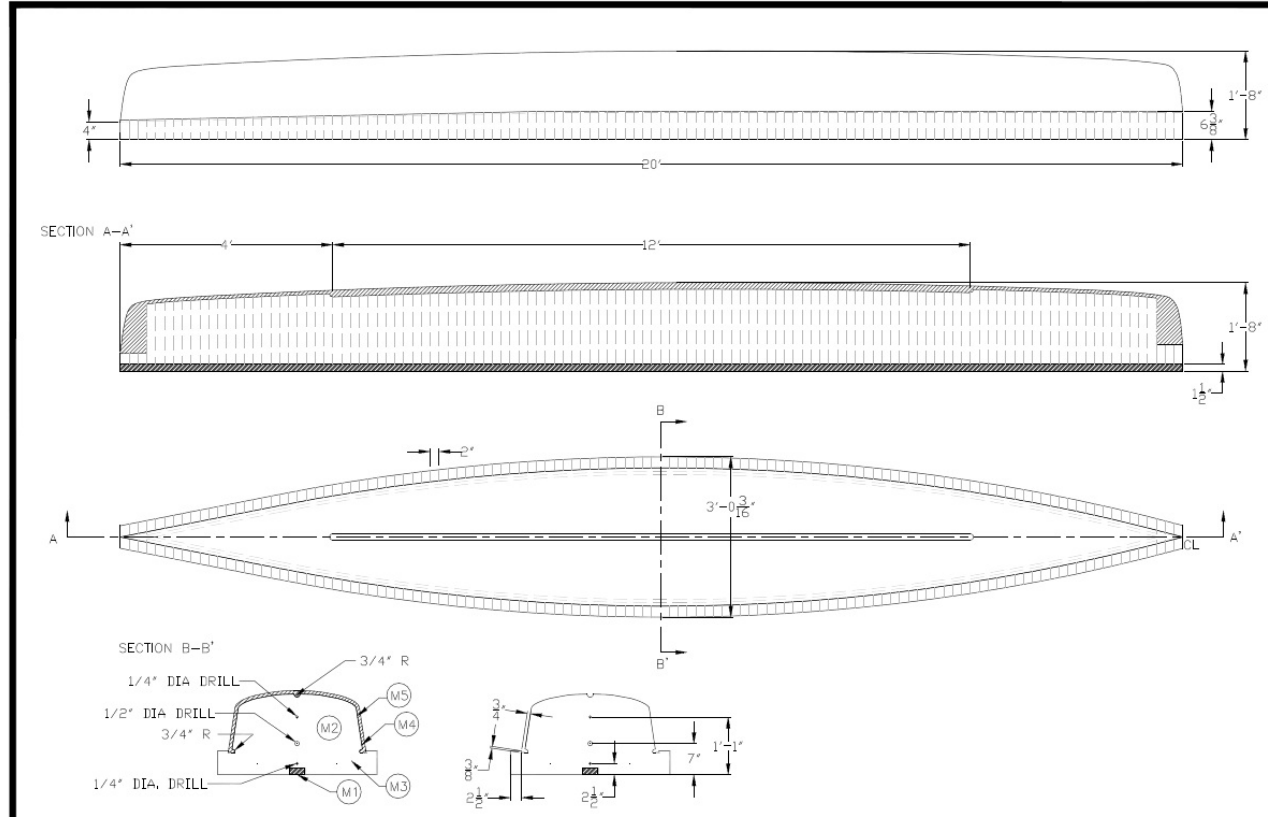


Project Schedule





Design Drawing

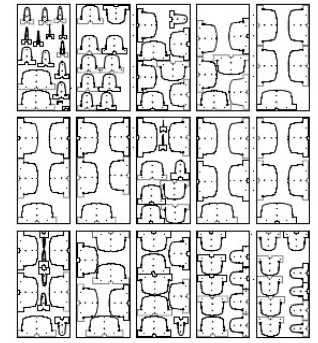


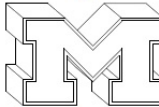
NOTES:
 3 DIMENSIONAL CROSS SECTIONS OF 2 INCH THICKNESSES ARE TO BE OBTAINED ALONG THE LENGTH OF THE CANOE USING RHINOCEROS 4.0, FOR FABRICATION USING A CNC ROUTER.
 ONCE ALIGNED ON FLAT, LEVEL SURFACE USING 2x4's AND A LASER SIGHT, THE FOAM CROSS SECTIONS ARE TO BE GLUED TOGETHER, SANDED SMOOTH AND COATED WITH DRYWALL COMPOUND. THE MOLD IS TO BE COVERED IN DUCT TAPE TO FACILITATE DEMOLDING.

MCCT BILL OF MATERIALS

ITEM	QTY.	DESCRIPTION
M1	3	LUMBER 2"x4"x8'
M2	15	FOAMBOARD 4'x8'x2"
M3	1	WOOD GLUE
M4	1	DRYWALL COMPOUND
M5	1	DUCT TAPE COATING

FORMWORK CUTPATHS SCALE 1/8":1'



Naval Architecture &

 Marine Engineering
 DATE: 1/29/2011

MCCT Canoe - "It's a Trap!"
 VESSEL DESIGNED FOR:
 ASCE NCCC
 DESIGNED AND DRAWN BY:
 Michigan Concrete Canoe Team
 SCALE: 1/2":1' SHEET 10 OF 10





Appendix A – References

ACI 318-08, “Building Code Requirements for Structural Concrete,” American Concrete Institute. (copyright 2008).

ASTM C 31/C 31M, “Standard Practice for Making and Curing Concrete Test Specimens in the Field,” ASTM International Book of Standards vol.04.02. (copyright 2005)

ASTM C33-03, “Standard Specification for Concrete Aggregates,” ASTM International Book of Standards vol.04.02. (copyright 2005).

ASTM C109/C109M-02, “Standard Test Method for Compressive Strength of Hydraulic Cement Mortars,” ASTM International Book of Standards vol.04.01. (copyright 2005).

ASTM C496, “Standard Test Method for Splitting Tensile Strength of Cylindrical Concrete Specimens” ASTM International Book of Standards vol. 04.03 (copyright 2005)

ASTM C150-04ae1, “Standard Specification for Portland Cement,” ASTM International Book of Standards vol.04.01. (copyright 2005).

“Ferrocement and Laminated Cementitious Composites,” Antoine E. Naaman. (copyright 2000).

“Poraver Product Specifications” (copyright Poraver North America, 2006)
< http://www.poraver.com/02rohstoff/pdf/product_specifications.pdf >
(accessed October 2009)

“3M Scotchlite Glass Bubbles: K and S series Product Information.” (copyright 3M 2006). <http://www.3m.com/microspheres/s_k_1.html> (accessed October 2009).



Appendix B – Mixture Proportions

Mixture ID: Grey Structural Mix				Design Proportions (Non SSD)		Actual Batched Proportions		Yielded Proportions		
Y _o	Design Batch Size (ft ³):									
	1									
Cementitious Materials				SG	Amount (lb/yd ³)	Volume (ft ³)	Amount (lb)	Volume (ft ³)	Amount (lb/yd ³)	Volume (ft ³)
CM1	Portland Cement Type I			3.15	383.08	1.949	14.19	0.072	367.53	1.87
CM2	GGBFS			2.50	268.16	1.719	9.93	0.064	257.27	1.65
CM3	RHA			2.16	114.92	0.853	4.26	0.032	110.25	0.82
Total Cementitious Materials:					766.16	4.521	28.38	0.167	735.051	4.337
Fibers										
F1	PVA Fiber			1.30	6.90	0.085	0.26	0.003	6.62	0.08
Total Fibers:					6.90	0.085	0.26	0.003	6.620	0.082
Aggregates										
A1	K15	Abs:	0.1	0.15	26.82	2.865	0.99	0.106	25.73	2.75
A2	Haydite	Abs:	10	0.80	50.57	1.013	1.87	0.038	48.52	0.97
A3	Bionic Bubbles	Abs:	3	0.59	91.17	2.476	3.38	0.092	87.47	2.38
A4	Poraver 0.5-1mm	Abs:	3	0.47	101.13	3.448	3.75	0.128	97.02	3.31
A5	Poraver 0.25-0.5mm	Abs:	3	0.55	67.42	1.964	2.50	0.073	64.68	1.88
Total Aggregates:					337.11	11.767	12.49	0.436	323.42	11.29
Water										
W1	Water for CM Hydration (W1a + W1b)				381.69	6.117	14.14	0.227	366.20	5.87
	W1a. Water from Admixtures			1.00	60.81		2.25		58.34	
	W1b. Additional Water				320.88		11.88		307.86	
W2	Water for Aggregates, SSD			1.00	12.88		0.48		12.35	
Total Water (W1 + W2):					394.57	6.32	14.61	0.234	378.55	6.07
Solids Content of Latex Admixtures and Dyes										
S1	Dow Liquid Latex Modifier			1.05	57.46	0.88	2.13	0.032	55.13	0.84
Total Solids of Admixtures:					57.46	0.88	2.13	0.032	55.129	0.841
Admixtures (including Pigments in Liquid Form)				% Solids	Dosage (fl oz/cwt)	Water in Admixture (lb/yd ³)	Amount (fl oz)	Water in Admixture (lb)	Dosage (fl oz/cwt)	Water in Admixture (lb/yd ³)
Ad1	Glenium 7500	8.8 lb/gal		5	3.64	1.82	1.03	0.067	3.49	1.75
Ad2	AE90	8.5 lb/gal		5	3.16	1.53	0.90	0.057	3.03	1.47
Ad3	Liquid Latex Modifier	8.8 lb/gal		50	218.1818	57.46	61.91	2.128	209.32	55.13
Water from Admixtures (W1a):						60.81		2.25		58.34
Cement-Cementitious Materials Ratio					0.500		0.500		0.500	
Water-Cementitious Materials Ratio					0.515		0.515		0.515	
Slump, Slump Flow, in .					4±1		3.000		4±1	
M	Mass of Concrete, lbs				1562.20		57.86		1498.77	
V	Absolute Volume of Concrete, ft ³				23.57		0.87		22.62	
T	Theoretical Density, lb/ft ³ = (M / V)				66.27		66.27		66.27	
D	Design Density, lb/ft ³ = (M / 27)				57.86					
D	Measured Density, lb/ft ³						55.51		55.51	
A	Air Content, % = [(T - D) / T x 100%]				12.69		16.24		16.24	
Y	Yield, ft ³ = (M / D)				27		1.042		27	
Ry	Relative Yield = (Y / Y _o)						1.042			



Mixture ID: White Structural Mix				Design Proportions (Non SSD)		Actual Batched Proportions		Yielded Proportions		
Y _o	Design Batch Size (ft ³):									
			1							
Cementitious Materials				SG	Amount (lb/yd ³)	Volume (ft ³)	Amount (lb)	Volume (ft ³)	Amount (lb/yd ³)	Volume (ft ³)
CM1	Portland Cement Type I			3.15	383.08	1.949	14.19	0.072	422.92	2.15
CM2	GGBFS			2.50	383.08	2.456	14.19	0.091	422.92	2.71
CM3	RHA			2.16	0.00	0.000	0.00	0.000	0.00	0.00
Total Cementitious Materials:					766.16	4.405	28.38	0.163	845.833	4.863
Fibers										
F1	PVA Fiber			1.30	6.90	0.085	0.26	0.003	7.62	0.09
Total Fibers:					6.90	0.085	0.26	0.003	7.618	0.094
Aggregates										
A1	K15	Abs:	0.1	0.15	27.58	2.947	1.02	0.109	30.45	3.25
A2	Haydite	Abs:	10	0.80	55.16	1.105	2.04	0.041	60.90	1.22
A3	Bionic Bubbles	Abs:	3	0.59	86.57	2.351	3.21	0.087	95.57	2.60
A4	Poraver 0.5-1mm	Abs:	3	0.47	96.53	3.291	3.58	0.122	106.57	3.63
A5	Poraver 0.25-0.5mm	Abs:	3	0.55	79.68	2.322	2.95	0.086	87.97	2.56
Total Aggregates:					345.52	12.016	12.80	0.445	381.45	13.27
Water										
W1	Water for CM Hydration (W1a + W1b)				381.14	6.108	14.12	0.226	420.78	6.74
	W1a. Water from Admixtures			1.00	60.81		2.25		67.13	
	W1b. Additional Water				320.33		11.86		353.64	
W2	Water for Aggregates, SSD			1.00	13.43		0.50		14.82	
Total Water (W1 + W2):					394.57	6.32	14.61	0.234	435.60	6.98
Solids Content of Latex Admixtures and Dyes										
S1	Dow Liquid Latex Modifier			1.05	57.46	0.88	2.13	0.032	63.44	0.97
Total Solids of Admixtures:					57.46	0.88	2.13	0.032	63.437	0.968
Admixtures (including Pigments in Liquid Form)				% Solids	Dosage (fl oz/cwt)	Water in Admixture (lb/yd ³)	Amount (fl oz)	Water in Admixture (lb)	Dosage (fl oz/cwt)	Water in Admixture (lb/yd ³)
Ad1	Glenium 7500	8.8 lb/gal		5	3.64	1.82	1.03	0.067	4.01	2.01
Ad2	AE90	8.5 lb/gal		5	3.16	1.53	0.90	0.057	3.49	1.69
Ad3	Liquid Latex Modifier	8.8 lb/gal		50	218.1818	57.46	61.91	2.128	240.87	63.44
Water from Admixtures (W1a):						60.81		2.25		67.13
Cement-Cementitious Materials Ratio					0.500		0.500		0.500	
Water-Cementitious Materials Ratio					0.515		0.515		0.515	
Slump, Slump Flow, in .					4±1		3.000		4±1	
M	Mass of Concrete. lbs				1570.61		58.17		1733.94	
V	Absolute Volume of Concrete, ft ³				23.71		0.88		26.17	
T	Theoretical Density, lb/ft ³ = (M / V)				66.25		66.25		66.25	
D	Design Density, lb/ft ³ = (M / 27)				58.17					
D	Measured Density, lb/ft ³						64.22		64.22	
A	Air Content, % = [(T - D) / T x 100%]				12.20		3.07		3.07	
Y	Yield, ft ³ = (M / D)				27		0.906		27	
Ry	Relative Yield = (Y / Y _o)						0.906			

Appendix C – Bill of Materials

Material	Quantity	Unit Cost	Total Price
Portland Cement Type I	70.1 lbs	\$0.037/lb	\$2.59
GGBFS	49.1 lbs	\$0.025/lb	\$1.23
RHA	21.0 lbs	\$0.16/lb	\$3.36
PVA Fiber	1.3 lbs	\$2.27/lb	\$2.95
K15	4.9 lbs	\$7.77/lb	\$38.07
Haydite	9.3 lbs	\$0.05/lb	\$0.47
Bionic Bubbles	16.7 lbs	\$8.25/lb	\$137.80
Poraver 0.5-1 mm	18.5 lbs	\$0.85/lb	\$15.73
Poraver 0.25-0.5	12.3 lbs	\$0.85/lb	\$10.46
Dow Liquid Latex Modifier	21.0 lbs	\$8.41/lb	\$176.60
Glenium 7500	0.35 lbs	\$1.50/lb	\$0.53
AE90	0.29 lbs	\$0.50/lb	\$0.15
Fiberglass Mesh	83.9 sq ft	\$0.14/sq ft	\$11.75
Acid Wash	2 gal	\$9/gal	\$18.00
Stain	2 gal	\$82/gal	\$164.00
Sealer	2 gal	\$26/gal	\$52.00
Paint for Lettering	4 oz	\$2.50/oz	\$10.00
Foam Mold, Complete	1 mold	\$560/mold	\$560.00
Sand Paper	5 packs	\$30/pack	\$150.00
Total Production Cost			\$1,355.69